

Culvert Foundation Recommendation Letter Aluminum Arch Culvert @ -L- Sta. 13+58.00 over Richland Swamp Robeson County, North Carolina NCDOT Project No.: BP6.R005 S&ME Project No. 213634A

PREPARED FOR:

CDM Smith, Inc. 5400 Glenwood Ave, Suite 400 Raleigh, North Carolina 27612

PREPARED BY:

S&ME, Inc. 9751 Southern Pine Boulevard Charlotte, North Carolina 28273

October 11, 2022



October 11, 2022

CDM Smith, Inc. 5400 Glenwood Ave, Suite 400 Raleigh, North Carolina 27612

Attention: Adam Conrad, P.E. Project Manager

Reference:	Culvert Foundation Recommendation Letter		
	Aluminum Arch Culvert @ -L- S	Sta. 13+58.00 over Richland Swamp	
	NCDOT Project Number:	BP6.R005	
	County:	Robeson	
	S&ME Project No.:	213634A	
	NC PE Firm License No.:	F-0176	

Dear Mr. Conrad:

S&ME, Inc. (S&ME) has completed the authorized culvert foundation recommendation report for the abovereferenced project. Our services were performed in general accordance with the Agreement for Professional Services contract between CDM Smith, Inc and S&ME, dated February 17, 2022.

Project and Recommendations

We understand that existing pipe culvert, crossing Old Red Springs Road (SR 1303), is to be replaced with a 117inch x 79-inch Arch Culvert. The proposed culvert replacement will be approximately 51 feet long with a centerline invert elevation of 176.47 feet and slope of 1.78 percent.

Based on our subsurface exploration, the proposed culvert is planned to bear in alluvial soils. The Arch Culvert should be installed to bear on a minimum of 12 inches of foundation conditioning material in accordance with NCDOT Standard Specifications Section 414. A total of 49 tons of foundation conditioning material is anticipated.

Less than 0.1 inches of total settlement is expected. Therefore, no camber is required.



Culvert Foundation Recommendation Letter Aluminum Arch Culvert @ -L- Sta. 13+58.00 over Richland Swamp Robeson County, North Carolina S&ME Project No. 213634A

Recommended Plan Notes

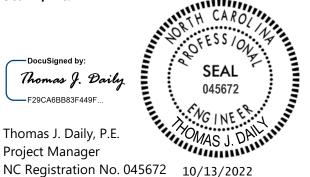
BACKFILL WITH SELECT MATERIAL, CLASS VI MEETING THE REQUIREMENTS OF SECTION 1016 OF THE STANDARD SPECIFICATIONS.

Closing

S&ME appreciates the opportunity to provide our services on this project. Please contact us if you have any questions regarding this report or if we may be of further assistance.

Sincerely,





Senior Review By: Kristen H. Hill, P.E., P.G.

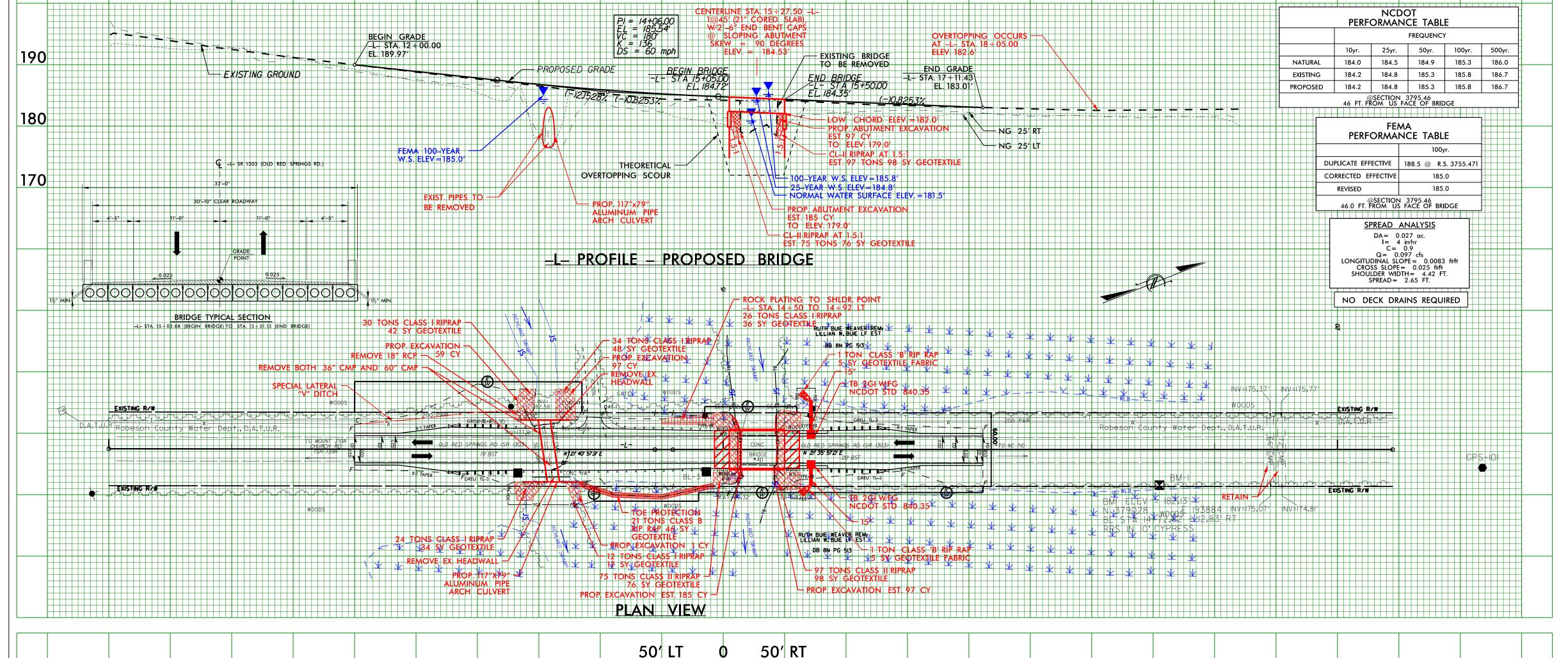
Ali Salehim

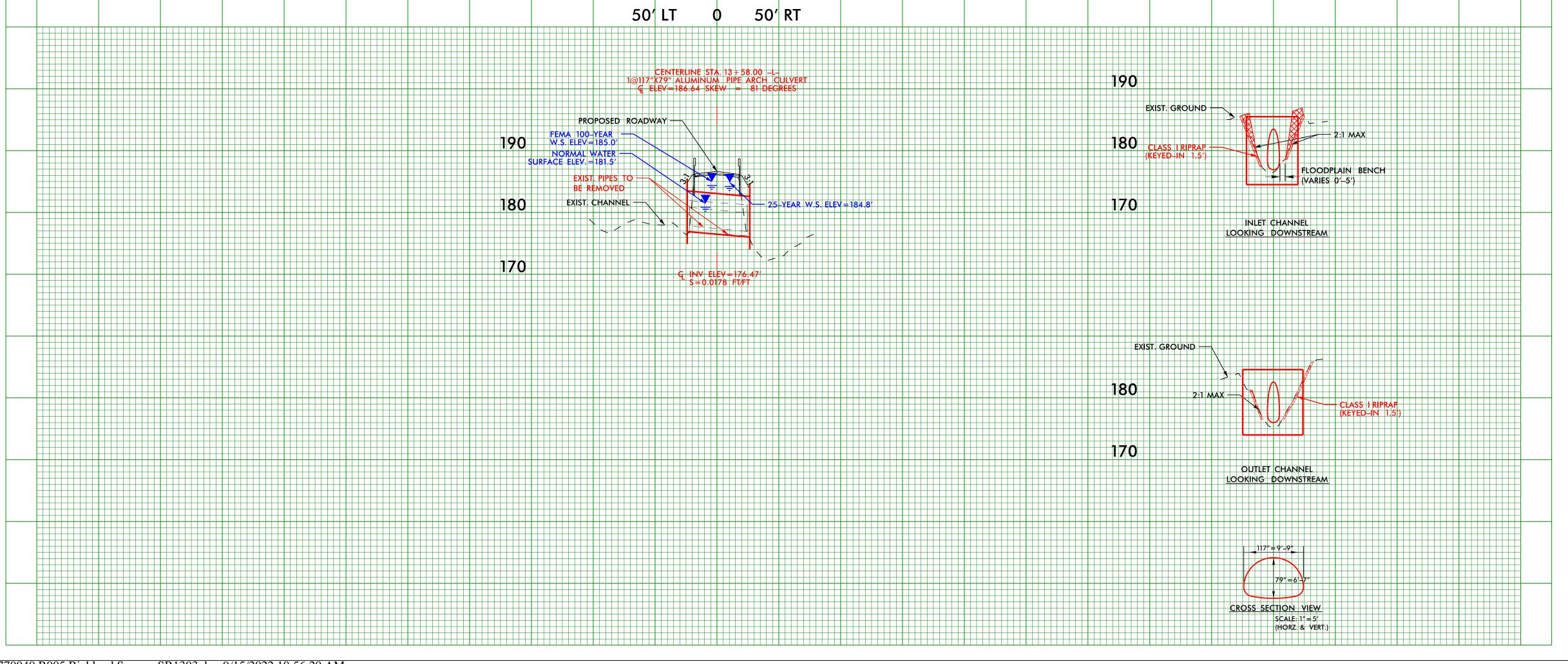
Ali Salehian, P.E. Project Engineer NC Registration No. 046104

Attachments

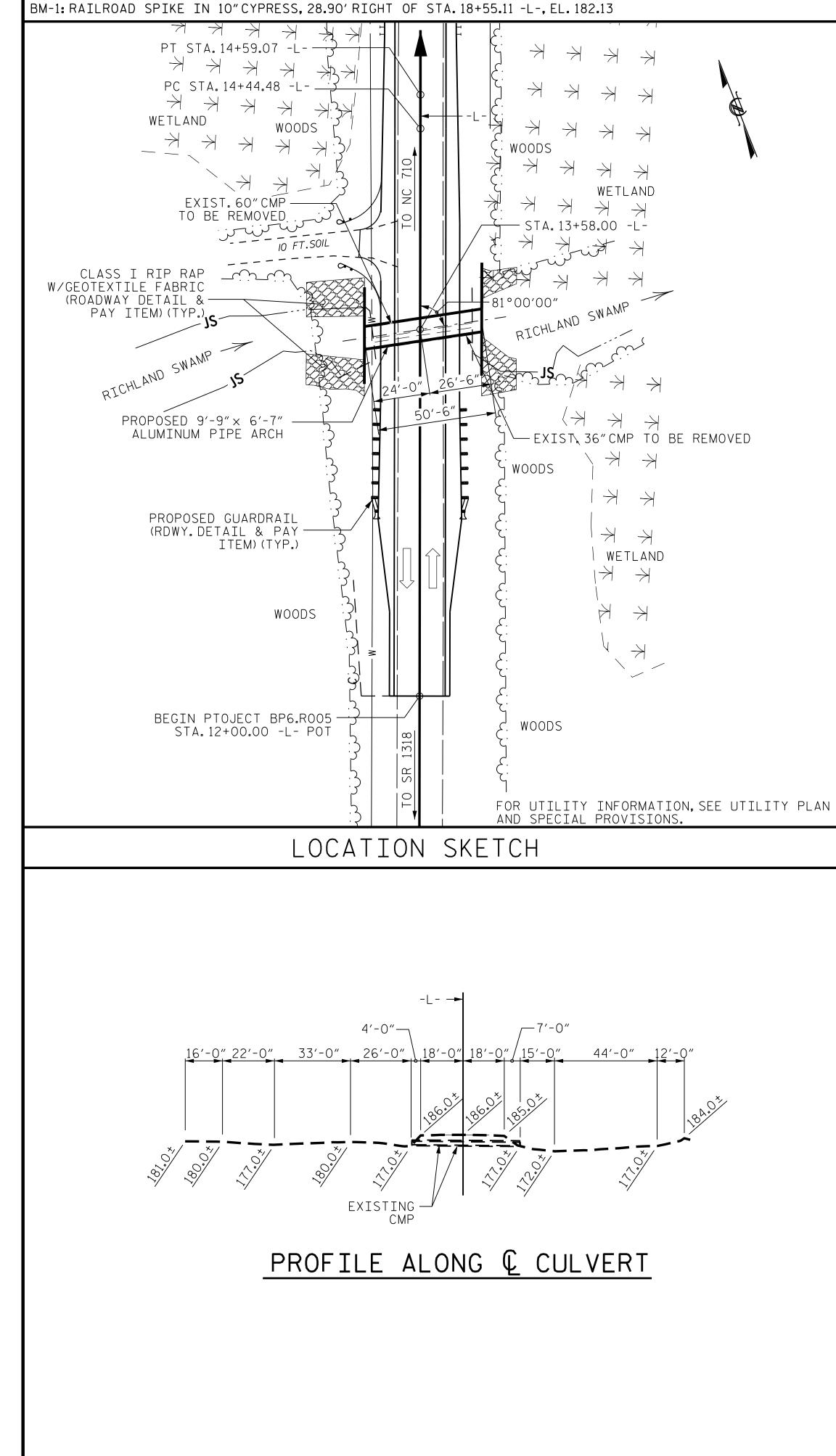
Culvert Survey & Hydraulic Design Report CDM Smith 85% Draft Culvert Plans FCM Quantity Calculations Settlement Calculations Attachments

F Reviewed by:	ls α Floodway Revision Required? UO, MOA TYPE 1
Project Engineer pousigned ADAM CONRAD, P.E.	Computed Scour : General <u>WA</u> ft. Contraction 6 ft. Local WA ft.
Assisted by: PRABHASH JOSHI, El Date 9/15/2022 SEAL	** WATERWAY OPENING AREA IN PROPOSE CONDITION INCLUDES PROP. 45' BRIDGE, PROP. 45' B
Designed by: HEATHER HARKEURIDER, PE	Waterway Opening Provided Below: 250**s.f., 100yr W.S. Elev. 250**s.f., Total 250**_s.f., Total 250**_s.f.,
	500 2440 186.7 0.7 0.7
	NO INSURABLE STRUCTURES AT THE TIME OF THE PROJECT WILL BE ADVERSELY IMPACTED BY THIS
S	
The	BEYOND THE BRIDGE DID HAVE SOME WATER OVERTOPPING THE LOW POINT.
Inv.	MAINTENANCE SUPERVISOR THE STRUCTURE 770040 DID NOT GO UNDER WATER BUT ROAD
Z Z	* ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDING TO THE INFORMATION RECEIVED FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDINATION FROM STEVEN BLANTON STEVEN BLANTON, NCDOT BRIDGE * ACCORDINATION FROM STEVEN BLANTON, NCDOT BRIDGE * ACCORDINATION BLANTON BLANTON BLANTON STEVEN
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	T.0.2 ZA9-D3H bottaulic Desian Methods 5.0.7
	$Y_{s} = Y_{xx} - Y_{s}$ $Y_{s} = 12.0 - 4.6 = 7.4 \text{ ft}. SAY = 7'$
6.5	$V_{m} = \alpha(Y_{0}) = \alpha[Y_{0}] = \alpha$
	ABUTMENT SCOUR: OT FLOW (NCHRP 24–20 EQUATION)
	$Y_{s} = Y_{z} - Y_{o}$ Flood Study 100yr. Discharge 1189 WS Elev.: With With With With With With With With
	Y= Y [Q, /Q,]"[W, /W,]" OT FLOW: Y= 5.8 [126.2/65.3]" [45.0/44.4]" Established? Telon: Y= 5.8 [126.2/65.3]" [45.0/44.4]" Established?
Diect Diect	Manning's n: Left O.B. 0.115 Channel 0.05 Right O.B. 0.122 Source FEME /FIELD OBSERVATION
S o Lemborary Crossing Officient DETOUR	Channel Slope 0.015 fift Source DETAILED SURVEY Normal Water Surface Elev. 181.5 ft.
	THE DESIGN DISCHARGES WERE USED FOR PESIGN AND FEMA 100 YR DISCHARGE FOR FEMA Historical Scour Info. : General UA. It. Contraction UA. It. Local UA.
88 Uverbing 379028.1349 Ersting 1938861.1435 Elev 182.13' ft Datum: WAVD 88	DateKreqKreqKreqKreqKreqKredKredKredKred. of
Bench Mark is BM–1, STA 18+55.11, 28.90' RT,	
אַ Statewide Tier □ Kegional Tier □ Sub–Regional Tier ⊠ איז Statewide Tier □ געליאטא איז איז איז איז איז איז איז איז איז אי	Q ₁ = 550 (DA) ¹⁰⁰ = 2,443 CFS SAY 2,440 CFS Q ₁ = 550 (DA) ¹⁰⁰ = 2,443 CFS SAY 1,740 CFS Partice A Alloce Particle A SAY 2,440 CFS Particle A Period of Particle A SAY 2,440 CFS Particle A Period of Particle A SAY 2,440 CFS Particle A SAY 2,440 CFS
لد Latitude <u>34.79047</u> Longitude – 79.20421	Q _i = 309 (DA) ^{min} = 1,433 CFS SAY 1,740 CFS Q _{in} = 380 (DA) ^{min} = 1,433 CFS SAY 1,740 CFS Q _{in} = 380 (DA) ^{min} = 1,433 CFS SAY 1,740 CFS Q _{in} = 380 (DA) ^{min} = 1,433 CFS SAY 1,740 CFS Q _{in} = 380 (DA) ^{min} = 1,433 CFS SAY 1,740 CFS Q _{in} = 380 (DA) ^{min} = 1,433 CFS SAY 1,740 CFS Period of Porteyr. Source MAINTENANCE SUPERVISOR *yr.Source MAINTENANCE SUPERVISOR *yr.Source MAINTENANCE SUPERVISOR *
Recommended Location is (Up, At, Down) Stream from Existing Crossing.	ar. Discharge VA C.f.s. Date VA 7,154 CFS SAY 7,160 CFS (DA)™ = 1,154 CFS SAY 7,160 CFS (DA)™ = 1,154 CFS SAY 7,160 CFS
Recommended Width of Roadway 30'-10" CLEAR ROADWAY Skew AL	Gage Station No. NA Period of Records NA Period of Records NA
20 DEGREE	
	RURAL COASTAL PLAIN SIR 2009–5158 Design Control Elev. 184.8 ft. (25yr), 185.0 ft. (100 yr) Design Control Elev. 294.6 ft. (25yr), 185.0 ft. (100 yr)
B Kecommended Structures J@45' (21" CORED SLAB), W/ 2'-6" E.B. CAPS	
S Ou Highway (OLD RED SPRINGS RD) Between ИС 710 and SR 1318 (MOUNT ZION CHURCH RD)	NOLE: BANK2 AKE SUBWEKCED MELFAND2' AECELALED' MIDE AND STABLE
Z County ROBESON Bridge Over RICHLAND SWAMP Bridge Inv. No. 770040	Debris Potential: LowX Moderate
ی م I.D. No. SF–770040 Project No. BP6.R005 Proj. Station 75+27.50	PROPOSED ROADWAY Q
	Overtopping: Discharge 320 c.f.s. Frequency 2
רבופרו, א. כ. א פרבופרו, א. כ. גאנבופרו, א. כ.	
DIVISION OF HIGHWAYS	Wc.D (sto rota I dail trust at Classification (sto at 10 dail trust at 10 daile at 10 dail
	Design: Discharge 1160 c.f.s. Frequency 25 yr. Elev. 184.8 ft. River Basin LUMBER RIVER Character SWAMPY, RURAL
	WS EL. Taken @ River Station 3795.46 WS EL. Taken @ River Station 3795.46
	ATAD ATIZ
10+00 11+00 12+00 13+00	14+00 15+00 16+00 17+00 18+00





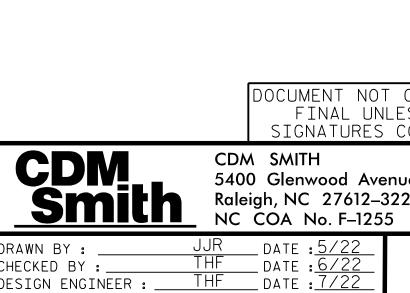
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ROADWAY DA	ТА	NOTES
GRADE PT.EL.@ STA.13+58.00 -L-	= 186.64′	ASSUMED LIVE L
BED ELEV.@ STA.13+58.00 -L- Roadway slope	= 176.47′ = 3:1	PIPE ARCH CULV 2'-3"AND A MAX
		3″Ø WEEP HOLES
HORIZONTAL CURV P.I. STA. = 14+51.77 -L- △ = 0°-05'-00.9"(LT.)		THE CONTRACTOF CULVERT BEFORE TAKE CARE OF T
$D = 0^{\circ} - 34' - 22.6''$ $L = 14.59'$ $T = 7.29'$		ALL MATERIALS SPECIFICATIONS
R = 10,000.00'		THE DETAILS SH Details, design
HYDRAULIC DA	ТА	REQUIREMENTS O ARE SEALED BY
	= 1160 CFS = 25 YRS. = 184.8′	UNLESS OTHERWI All structural
DRAINAGE AREA	= 12.9 SQ.MI. = 1740 CFS	GUARDRAIL POST TO ENSURE ADEC
BASE HIGH WATER ELEVATION	= 185.8′	ROADWAY DETAIL
OVERTOPPING FLOO	D DATA	EXCAVATE 1 FOO CONDITIONING M SPECIFICATIONS
OVERTOPPING DISCHARGE		BACKFILL CULVE SPECIFICATIONS
FREQUENCY OF OVERTOPPING FLOOD OVERTOPPING FLOOD ELEVATION		FOR ALUMINUM H 13+58.00 -L- SP
* OVERTOPPING OCCURS AT (AT STA	.18+05.00 -L-	FOR SUBMITTAL
		FOR CONSTRUCT
TOTAL STRUCTURE QUAN	NITITES	FOR FALSEWORK
REMOVAL OF EXISTING STRUCTURE	LUMP SUM	FOR CRANE SAFE
CULVERT EXCAVATION	LUMP SUM	NO PRECAST REI
FOUNDATION CONDITIONNING MATERIAL	97 TONS	
ALUMINUM PIPE ARCH	LUMP SUM	
FLOWABLE FILL	26.6 C.Y.	THE ALUMINUM E Foundation con



DESIGN ENGINEER :

LOAD -----HL-93 OR ALTERNATE LOADING LVERT IS TO BE DESIGNED FOR A MINIMUM FILL DEPTH OF AXIMUM OF 3'-5". ES INDICATED TO BE IN ACCORDANCE WITH THE SPECIFICATIONS. OR SHALL CHECK THE LENGTH AND ELEVATION OF THE PIPE ARCH RE STAKING IT OUT TO MAKE CERTAIN THAT IT WILL PROPERLY THE FILL. SHALL MEET THE REQUIREMENTS OF THE NCDOT STANDARDS NS FOR ROADS AND STRUCTURES DATED JANUARY 2018. SHOWN ARE FOR GENERAL LAYOUT ONLY. THE SUPPLIER SHALL PROVIDE GN AND RATING SHEET FOR REVIEW AND APPROVAL THAT MEET THE OF AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12, AND A NORTH CAROLINA REGISTERED PROFESSIONAL ENGINEER. NISE INDICATED, THE SUPPLIER SHALL DETAIL, DESIGN, AND FURNISH AL ELEMENTS AND HARDWARE. ST LOCATIONS SHALL BE DETERMINED IN THE FIELD BY THE ENGINEER EQUATE COVER AND INSTALLATION.FOR CULVERT 25 FT OR LESS, SEE IL DRAWING 862D01 AS OPTIONAL GUARDRAIL PLACEMENT. OOT BELOW PIPE ARCH CULVERT AND REPLACE WITH FOUNDATION MATERIAL IN ACCORDANCE WITH SECTION 414 OF THE STANDARD VERT IN ACCORDANCE WITH SECTION 414 OF THE STANDARD NS OR AS RECOMMENDED BY ALUMINUM PIPE ARCH CULVERT MANUFACTURER. PIPE ARCH CULVERT, SEE ALUMINUM PIPE ARCH CULVERT AT STATION SPECIAL PROVISIONS. OF WORKING DRAWINGS, SEE SPECIAL PROVISIONS. TION SEQUENCE SEE EROSION CONTROL PLANS. AND FORMWORK, SEE SPECIAL PROVISIONS.

FETY, SEE SPECIAL PROVISIONS. EINFORCED BOX CULVERT OPTION WILL BE ALLOWED.

FOUNDATION NOTE

BOX CULVERT SHALL BE CONSTRUCTED WITH 12 INCHES OF FOUNDATION CONDITIONING MATERIAL PLACED BELOW THE BOTTOM OF CULVERT.

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Draf			
10/04/20)22 2:54	:13 PM	

PROJECT	NO.	BP6.	R005
ROB			_COUNTY
STATTON.	13+		

SHEET 1 OF 3

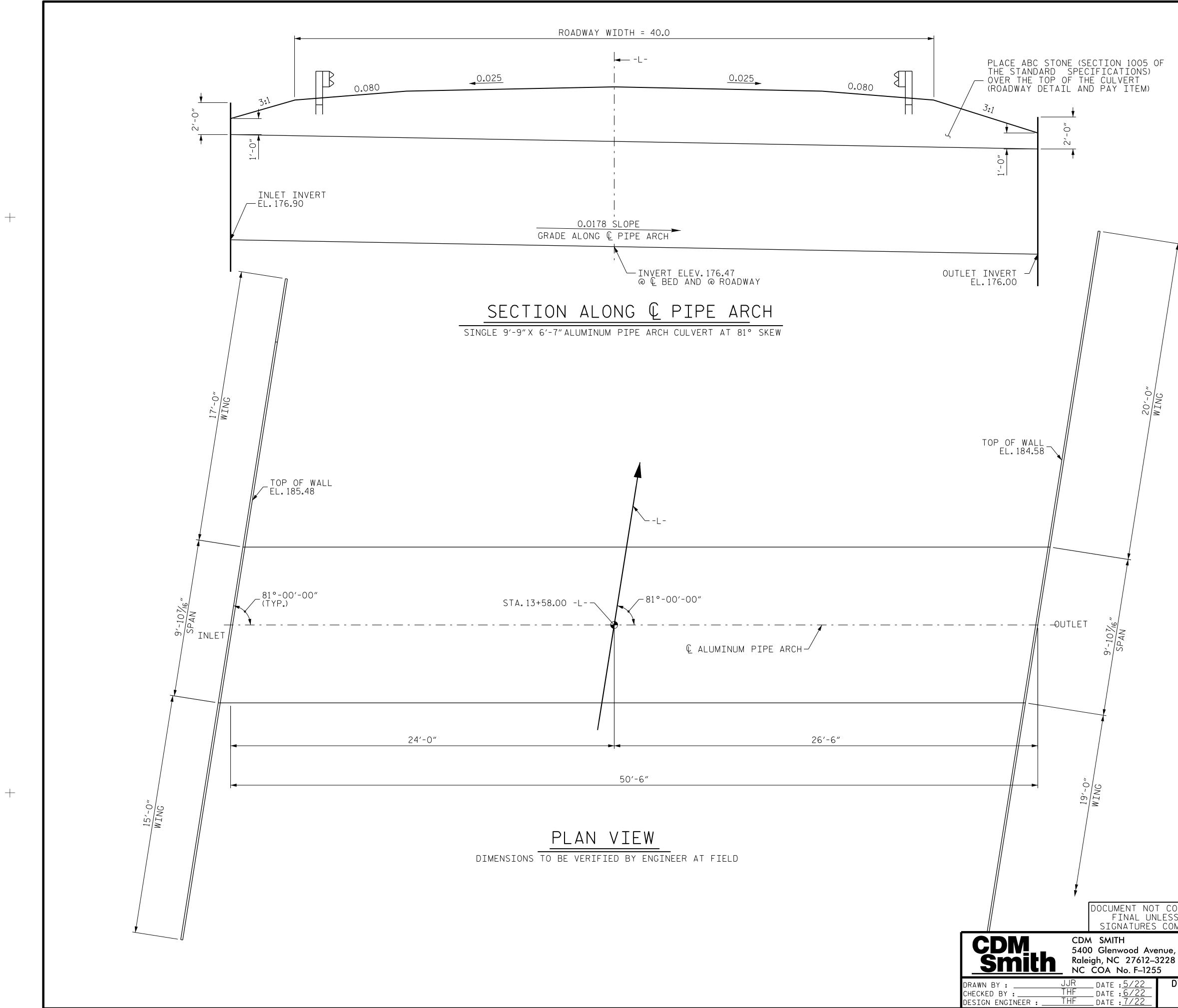
STATE OF NORTH CAROLINA DEPARTMENT OF TRANSPORTATION RALEIGH

SINGLE 9'-9" X 6'-7" ALUMINUM PIPE ARCH

81° SKEW

REVISIONS					SHEET NO.	
N0.	BY:	DATE:	N0.	BY:	DATE:	<u>C-I</u>
1			3			TOTAL SHEETS
2			4			3

CONSIDERED SS ALL COMPLETED	
ue, Suite 400 28	
DWG, No.	



NOTES:

MINIMUM EMBEDMENT ALONG THE BASE OF WALL SHALL BE 3'-O", INCLUDING 2'-O" OF FLOWABLE FILL SEE DETAIL SHEET C-3.

CONTRACTOR MUST SUBMIT SEALED SHOP DRAWINGS FOR ALUMINUM PIPE ARCH & HEADWALLS TO NCDOT FOR APPROVAL PRIOR TO CONSTRUCTION.

BACKFILL WITH NATIVE MATERIAL TO SILL HEIGHT IN THE CULVERT. NATIVE MATERIAL BETWEEN SILLS IN THE CULVERT SHALL PROVIDE A CONTINUOUS FLOW CHANNEL.

NATIVE MATERIAL CONSISTS OF MATERIAL THAT IS EXCAVATED FROM THE STREAM OR FLOODPLAIN AT THE PROJECT SITE DURING CONSTRUCTION.ONLY MATERIAL THAT IS EXCAVATED FROM THE STREAM BED MAY BE USED TO LINE CULVERT.

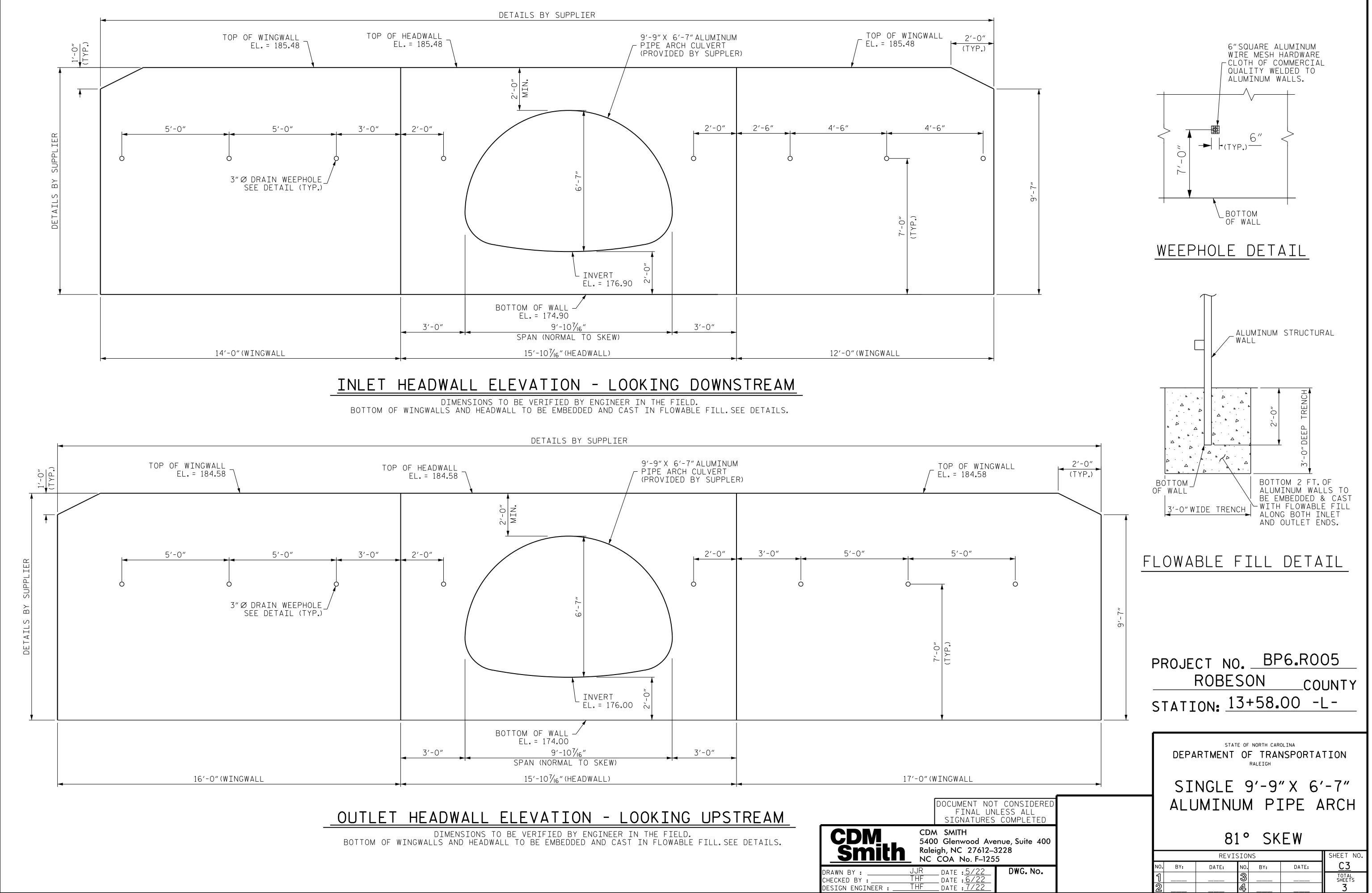
RIP RAP MAY BE USED TO SUPPLEMENT THE NATIVE MATERIAL IN THE CULVERT. IF RIP RAP IS USED TO LINE THE FLOW CULVERT BARREL.NATIVE MATERIAL SHOULD BE PLACED ON TOP TO FILL VOIDS AND PROVIDE A FLAT SURFACE FOR ANIMAL PASSAGE.

NATIVE MATERIAL IS SUBJECT TO APPROVAL BY THE ENGINEER AND MAY BE SUBJECT TO PERMIT CONDITIONS.

	PROJECT NO. <u>BP6.R005</u> <u>ROBESON</u> COUNTY STATION: <u>13+58.00</u> -L-		
	SHEET 2 OF 3 STATE OF NORTH CAROLINA		
	DEPARTMENT OF TRANSPORTATION RALEIGH		
	SINGLE 9'-9"X 6'-7"		
ONSIDERED S ALL MPLETED	ALUMINUM PIPE ARCH		
, Suite 400	81° SKEW		
	REVISIONS SHEET NO. NO. BY: DATE: NO. BY: DATE: C-2		
DWG.No.	10. BT: DATE: DATE: 1 3 TOTAL SHEETS 2 4 3		

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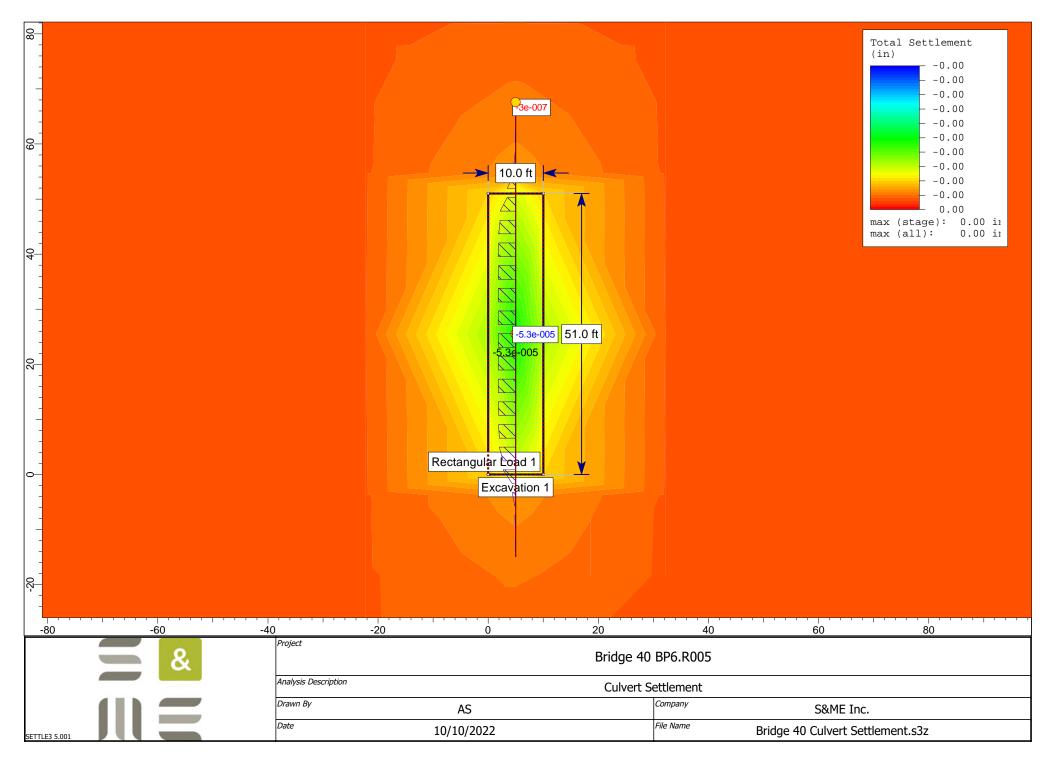
Culvert Undercut Quantities Box Culvert over Richland Swap



Alluminum Pipe Arch Culvert (1 @ 117" x 79")

Foundation Conditioning Material	
Beneath Culvert Footprint	
Single Culvert Inside Width	9.75
Number of Culverts	1
Number of Culvert Outside Walls	2
Number of Culvert Internal Divisions	0
Thickness of Walls & Divisions	N/A
Total Culvert(s) Outside Width	9.75
Culvert(s) Length (ft)	51
Per Structure Memo, UC to Outer + 4 feet	
UC Outside Width (ft)	13.75
UC depth (ft)	1
volume beneath culvert (ft^3)	701.25
volume beneath culvert (cy)	25.97
Reqd. Foundation Conditioning Material for Culvert(s) (tons)	49.5
Reqd. Foundation Conditioning Material for Culvert(s) (tons)	49
Per Structure Memo, 1.904 tons/cy	1.904

Per Structure Memo, do not include FCM quantity for standard turned-back wings



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Settle3 Analysis Information Bridge 40 BP6.R005

Project Settings

Document Name	Bridge 40 Culvert Settlement.s3z
Project Title	Bridge 40 BP6.R005
Analysis	Culvert Settlement
Author	AS
Company	S&ME Inc.
Date Created	10/10/2022
Stress Computation Method	Boussinesq
Minimum settlement ratio for subgrade modulus	0.9

Use average properties to calculate layered stresses

Improve consolidation accuracy

Ignore negative effective stresses in settlement calculations

Stage Settings

Stage #	Name
1	Excavate
2	Culvert
3	Traffic

Results

Time taken to compute: 0.0356957 seconds

Stage: Excavate

Data Type	Minimum	Maximum
Total Settlement [in]	-0.000113616	1.60535e-007
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	-0.000113616	1.60535e-007
Loading Stress ZZ [ksf]	-1.03	1.2027e-006
Loading Stress XX [ksf]	-0.953823	0.0362252
Loading Stress YY [ksf]	-0.678299	0.285732
Effective Stress ZZ [ksf]	-2.22045e-016	2.18599
Effective Stress XX [ksf]	-0.298423	1.28202
Effective Stress YY [ksf]	-0.0228991	1.30948
Total Stress ZZ [ksf]	-2.22045e-016	3.98
Total Stress XX [ksf]	-0.298423	2.97324
Total Stress YY [ksf]	-0.0228991	2.99428
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-1.67135e-006	4.7661e-009
Pore Water Pressure [ksf]	0	1.9656
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	0.00605	2.18317
Over-consolidation Ratio	1	133.508
Void Ratio	0	0
Hydroconsolidation Settlement [in]	0	0
Undrained Shear Strength	-0.0124414	4.8108e-008

Stage: Culvert

Data Type	Minimum	Maximum
Total Settlement [in]	-5.29471e-005	1.60702e-007
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	-5.29471e-005	1.60702e-007
Loading Stress ZZ [ksf]	-0.48	1.2027e-006
Loading Stress XX [ksf]	-0.4445	0.0168816
Loading Stress YY [ksf]	-0.316101	0.133157
Effective Stress ZZ [ksf]	0	2.24431
Effective Stress XX [ksf]	0	1.28522
Effective Stress YY [ksf]	0	1.29801
Total Stress ZZ [ksf]	0	3.98
Total Stress XX [ksf]	0	2.973
Total Stress YY [ksf]	0	2.98281
Modulus of Subgrade Reaction (Total) [ksf/ft]	-172221	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	-172221	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-7.78883e-007	4.7661e-009
Pore Water Pressure [ksf]	0	1.9656
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	0.00605	2.24159
Over-consolidation Ratio	1	1.36511
Void Ratio	0	0
Hydroconsolidation Settlement [in]	0	0
Undrained Shear Strength	-0.0128745	4.8108e-008

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Stage: Traffic

Data Type	Minimum	Maximum
Total Settlement [in]	-5.29471e-005	1.60702e-007
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	-5.29471e-005	1.60702e-007
Loading Stress ZZ [ksf]	-0.48	1.2027e-006
Loading Stress XX [ksf]	-0.4445	0.0168816
Loading Stress YY [ksf]	-0.316101	0.133157
Effective Stress ZZ [ksf]	0	2.24431
Effective Stress XX [ksf]	0	1.28522
Effective Stress YY [ksf]	0	1.29801
Total Stress ZZ [ksf]	0	3.98
Total Stress XX [ksf]	0	2.973
Total Stress YY [ksf]	0	2.98281
Modulus of Subgrade Reaction (Total) [ksf/ft]	-172221	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	-172221	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-7.78883e-007	4.7661e-009
Pore Water Pressure [ksf]	0	1.9656
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	0.00605	2.24159
Over-consolidation Ratio	1	1.36511
Void Ratio	0	0
Hydroconsolidation Settlement [in]	0	0
Undrained Shear Strength	-0.0128745	4.8108e-008

Loads

1. Rectangular Load: "Rectangular Load 1"

Length	10 ft
Width	51 ft
Rotation angle	0 degrees
Load Type	Flexible
Area of Load	510 ft ²
Load	0.55 ksf
Depth	10 ft
Installation Stage	Culvert

Coordinates

X [ft]	Y [ft]
2.66454e-015	7.10543e-015
10	7.10543e-015
10	51
2.66454e-015	51

Excavations

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1. Excavation: "Excavation 1"

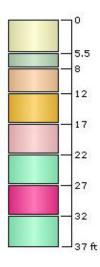
Depth 10 ft Installation Stage Excavate

Coordinates

X [ft]	Y [ft]
10	4.26326e-014
10	51
2.66454e-015	51
2.66454e-015	4.26326e-014

Soil Layers

Layer #	Туре	Thickness [ft]	Depth [ft]
1	A-2-4 (Fill)	5.5	0
2	A-7-5 (Alluv)	2.5	5.5
3	A-3 (Alluv)	4	8
4	A-2-4 (Alluv)	5	12
5	A-6 (CP)	5	17
6	A-2-4 (CP)	5	22
7	A-7-6 (CP)	5	27
8	A-2-4 (CP)	5	32



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Soil Properties

Property	A-2-4 (Fill)	A-7-5 (Alluv)	A-3 (Alluv)	A-2-4 (Alluv)
Color				
Unit Weight [kips/ft ³]	0.11	0.09	0.1	0.12
Saturated Unit Weight [kips/ft ³]	0.11	0.09	0.1	0.12
ко	0.5	0.5	0.5	0.5
Immediate Settlement	Disabled	Disabled	Enabled	Enabled
Es [ksf]	-	-	250	600
Esur [ksf]	-	-	2.5e+007	600000
Undrained Su A [kips/ft2]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Property	A-6 (CP)	A-2-4 (CP)	A-7-6 (CP)
Color			
Unit Weight [kips/ft ³]	0.105	0.115	0.095
Saturated Unit Weight [kips/ft ³]	0.105	0.115	0.095
KO	0.5	0.5	0.5
Immediate Settlement	Enabled	Enabled	Enabled
Es [ksf]	150	250	40
Esur [ksf]	1.5e+006	2.5e+007	4e+007
Undrained Su A [kips/ft2]	0	0	0
	0	v	U
Undrained Su S	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8
Piezo Line ID	1	1	1

ΠΞ

Groundwater

Groundwater method Piezometric Lines Water Unit Weight 0.0624 kips/ft³

Piezometric Line Entities

ID	Depth (ft)
1	5.5 ft

Query Points

Point #	Query Point Name	(X,Y) Location	Number of Divisions
1	Query Point 1	5, 25.5	Auto: 79

Query Lines

Line #	Query Line Name	Start Location	End Location	Horizontal Divisions	Vertical Divisions
1	Query Line 1	5, 67.5892	5, -14.8398	20	Auto: 77

Field Point Grid

Number of points	307
Expansion Factor	2

Grid Coordinates

X [ft]	Y [ft]
305	201
305	-150
-295	-150
-295	201